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# ***U.S. PATENT APPLICATION***

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***Invention:*** LOW-E COATING WITH HIGH VISIBLE TRANSMISSION

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## ***SPECIFICATION***

## TITLE OF THE INVENTION

### LOW-E COATING WITH HIGH VISIBLE TRANSMISSION

#### RELATED APPLICATION

**[0001]** This application is related to U.S. Patent Application Serial No. 09/794,224.

#### BACKGROUND AND SUMMARY OF THE INVENTION

**[0002]** The 09/794,224 application discloses coated articles having the following layer stack, as shown in Figure 1 herein, from the glass substrate outwardly:

Table 1: Example Materials/Thicknesses

Layer	Preferred Range (Å)	More Preferred (Å)	Example (Å)
Substrate (1-10 mm)			
TiO <sub>2</sub>	0-400 Å	50-250 Å	100 Å
Si <sub>x</sub> N <sub>y</sub>	0-400 Å	50-250 Å	170 Å
NiCrO <sub>x</sub>	5-100 Å	10-50 Å	18 Å
Ag	50-250 Å	80-120 Å	105 Å
NiCrO <sub>x</sub>	5-100 Å	10-50 Å	16 Å
SnO <sub>2</sub>	0-800 Å	500-850 Å	650 Å
Si <sub>x</sub> N <sub>y</sub>	0-800 Å	50-250 Å	170 Å
NiCrO <sub>x</sub>	5-100 Å	10-50 Å	18 Å
Ag	50-250 Å	80-120 Å	105 Å
NiCrO <sub>x</sub>	5-100 Å	10-50 Å	16 Å
SnO <sub>2</sub>	0-500 Å	100-300 Å	150 Å

Si<sub>3</sub>N<sub>4</sub>

0-500 Å

100-300 Å

250 Å

[0003] In other embodiments of 09/794,224, the bottom titanium oxide layer may be removed or replaced with a silicon nitride layer.

[0004] While the aforesaid coated articles described in the 09/794,224 application provide good color, and good ultraviolet (UV) and/or infrared (IR) reflection, increased visible transmission and/or reduced visible reflection would sometimes be desirable.

[0005] Neutral color is also desirable for coated articles in certain applications. Many conventional methods of making color of a coated article more neutral result in decreased visible transmission and/or increased visible reflection. Heretofore, it has been difficult to increase visible transmission and reduce visible reflection, while at the same time providing or maintaining rather neutral color and satisfactory solar control or thermal characteristics. Whether a color is "neutral" or not is subjective, and is a function of personal taste. However, generally speaking, color moving toward a neutral color target (e.g.,  $a^*=0$ ,  $b^*=0$ , or some other neutral color target such as transmissive  $a^*=-2$  and transmissive  $b^*=-3.4$ ) is desired, although such targets do not have to be met in all embodiments of this invention.

[0006] In view of the above, it is an object of certain embodiments of this invention to provide a solar controlling coated article (i.e., an article including at least one and preferably two or more layers such as Ag and/or Au for reflecting IR and/or UV) having increased visible transmission and/or reduced visible reflectance. In certain example non-limiting embodiments of this invention, it is an object to combine such high visible transmission and/or reduced visible reflection with neutral color of the coated article. Alternatively, the use of an improved anti-reflection layer(s) system(s) may enable coatings to have or utilize more robust contact layer(s) (e.g., thicker for better durability) and/or thicker silver (Ag) layer(s) (i.e., improved thermal performance) while maintaining similar transmission characteristics if increased transmission is not a most desired feature (e.g., if durability is a most desired feature).

[0007] Another object of this invention is to fulfill one or more of the above-listed objects and/or needs.

## BRIEF DESCRIPTION OF THE DRAWINGS

[0008] FIGURE 1 is a cross sectional view of a coated article according to an embodiment of this invention, as disclosed in the 09/794,224 application.

[0009] FIGURE 2 is a cross sectional view of a coated article according to an embodiment of this invention.

[0010] FIGURE 3 is a cross sectional view of a coated article according to another embodiment of this invention.

[0011] FIGURE 4 is a cross sectional view of a coated article according to another embodiment of this invention.

[0012] FIGURE 5 is a cross sectional view of a coated article according to another embodiment of this invention.

[0013] FIGURE 6 is a cross sectional view of a coated article according to another embodiment of this invention.

[0014] FIGURE 7 is a cross sectional view of a coated article according to another embodiment of this invention.

[0015] FIGURE 8 is a cross sectional view of a coated article according to another embodiment of this invention.

[0016] FIGURE 9 is a cross sectional view of a coated article according to another embodiment of this invention.

[0017] FIGURE 10 is a cross sectional view of a coated article according to another embodiment of this invention.

[0018] FIGURE 11 is a cross sectional view of a coated article according to another embodiment of this invention.

[0019] FIGURE 12 is a cross sectional view of a coated article according to another embodiment of this invention.

[0020] FIGURE 13 is a cross sectional view of a coated article according to another embodiment of this invention.

[0021] FIGURE 14 is a cross sectional view of a coated article according to another embodiment of this invention.

[0022] FIGURE 15 is a cross sectional view of a coated article according to another embodiment of this invention.

[0023] FIGURE 16 is a cross sectional view of a coated article according to another embodiment of this invention.

[0024] FIGURE 17 is a cross sectional view of a coated article according to another embodiment of this invention.

#### DETAILED DESCRIPTION OF EXAMPLE EMBODIMENTS OF THE INVENTION

[0025] The instant invention relates to coated articles which may be used in applications including but not limited to insulating glass (IG) window units, monolithic windows, skylight windows, and/or any other type of window. Coated articles according to this invention include an improved anti-reflection layer(s) system for reducing visible reflectance and/or increasing visible transmission in coated articles that provide solar control (e.g., IR and/or UV reflection) functionality. Surprisingly, in certain example embodiments it has been found that certain anti-reflection layer(s) systems of the instant invention can both: (a) improve visible transmission and/or reduce visible reflectance, while at the same time (b) achieving an acceptable neutral color of the resulting coated article.

[0026] Fig. 2 is a cross sectional view of a coated article according to an embodiment of this invention. The coated article of Fig. 2, like all other coated articles herein, may be used in any of the aforesaid applications (e.g., architectural windows, etc.). The coated article of Fig. 2 includes from the glass substrate outwardly (all indices of refraction "n" at 550 nm):

glass ( $n=1.51$ )

titanium oxide (e.g.,  $\text{TiO}_2$ ) ( $n=2.1$  to  $2.7$ , preferably  $n=2.4$  to  $2.65$ )

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

silver (Ag)

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

titanium oxide (e.g.,  $\text{TiO}_2$ ) ( $n=2.1$  to  $2.7$ , preferably  $n=2.4$  to  $2.65$ )

tin oxide (e.g.,  $\text{SnO}_2$ ) ( $n=1.8$  to  $2.2$ , preferably  $n=2.0$ )

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

silver (Ag)

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

titanium oxide (e.g.,  $\text{TiO}_2$ ) ( $n=2.1$  to  $2.7$ , preferably  $n=2.4$  to  $2.65$ )

tin oxide (e.g.,  $\text{SnO}_2$ ) ( $n=1.8$  to  $2.2$ , preferably  $n=2.0$ )

silicon oxide (e.g.,  $\text{SiO}_2$ ) ( $n=1.4$  to  $1.7$ , preferably  $n=1.45$ )

air ( $n=1.0$ )

**[0027]** As shown in Fig. 2, the contact layers (i.e.,  $\text{NiCrO}_x$  layers) surround and contact the IR reflecting Ag layers. The  $\text{NiCrO}_x$  layers herein are called "contact" layers because they each contact an IR reflecting layer (i.e., an Ag layer). The  $\text{NiCrO}_x$  contact layers provide the most immediate chemical protection for the Ag layer, and also serve as adhesion and/or nucleation layers. The contact layers may or may not be oxidation graded as described in the 09/794,224 application, in different embodiments of this invention. Moreover, instead of  $\text{NiCrO}_x$ , one or more of the contact layers may be of or include other material(s) including but not limited to  $\text{NiCr}$ ,  $\text{NiCrN}_x$ ,  $\text{NiCrO}_x\text{N}_y$ ,  $\text{ZnO}$ ,  $\text{Al}_2\text{O}_3$ ,  $\text{TiO}_2$ ,  $\text{ZnAlO}_x$ ,  $\text{Ni}$ ,  $\text{Cr}$ ,  $\text{CrN}_x$ ,  $\text{NiO}_x$ ,  $\text{NbO}_x$ , any combination thereof, and/or the like. Moreover, in any embodiment herein, materials such as titanium oxide or niobium oxide could even serve as top contact layers (i.e., above Ag layer(s)), in addition to dielectrics herein. Example thicknesses of the contact layers, and other layers herein, are discussed above in the Background and Summary section of this application. The above applies to contact layers in the Fig. 1-17 embodiments.

**[0028]** Instead of Ag, other metallic IR reflecting materials (e.g., Au, Ag alloys, Au alloys, etc.) may be used for one or more of the IR reflecting layers (this applies to the Fig. 1-17 embodiments). The thickness of the metallic Ag layers (IR

reflecting layers) is chosen in order to achieve the desired thermal performance (see example thickness ranges above). For example, the Ag layer may be from about 50-250 Å thick, in order to achieve sheet resistance ( $R_s$ ) (before and/or after heat treatment) of less than or equal to 10.0 ohms/square, more preferably less than or equal to 8.0 ohms/square, even more preferably less than or equal to 5.0 ohms/square, and most preferably less than or equal to 4.0 ohms/square. In a similar manner, the Ag layer(s) thickness(es) are chosen so that the coating (or coated article) has a normal emissivity ( $E_n$ ) of no greater than 0.08, more preferably no greater than 0.06, and most preferably no greater than 0.05 (before and/or after heat treatment). The aforesaid emissivity and sheet resistance characteristics apply to the Fig. 1-17 embodiments.

**[0029]** The IR reflecting and contact layers of the Fig. 2 coating (and the Fig. 3-17 coatings) are discussed in the 09/794,224 application (incorporated herein by reference), and are not discussed herein for reasons of simplicity. See the thicknesses/materials described in the 09/794,224 in this regard. The focus herein lies with the provision of dielectric layers which are utilized in order to: (a) increase visible transmission, (b) decrease visible reflection (e.g., glass side), and/or (c) provide neutral color. With respect to the Fig. 2 embodiment in particular, it will be shown below that the dielectric layers used therein (compared to in Fig. 1) result in a significant increase in visible transmission combined with a decrease in visible reflectance (glass and/or film side). This is beneficial.

**[0030]** It can be seen that the Fig. 2 embodiment of this invention differs from Fig. 1 in that (a) the bottom silicon nitride layer from Fig. 1 has been removed, (b) a titanium oxide layer has been added in the middle portion M, (c) the middle silicon nitride layer from Fig. 1 has been removed, (d) titanium oxide and silicon oxide layers have been added to the top portion T of the coating in Fig. 2, and (e) the top silicon nitride layer from Fig. 1 has been removed. By using silicon oxide (i.e., stoichiometric  $\text{SiO}_2$ , or alternatively a non-stoichiometric form) over the top tin oxide layer, and by utilizing the titanium oxide (i.e., stoichiometric  $\text{TiO}_2$ , or alternatively a non-stoichiometric form such as  $\text{TiO}_{1.50-1.99}$ ) layers as illustrated, the coating (layer system) can be characterized by the top dielectric portion T having an effective index

of refraction  $n$  less than that of middle dielectric portion M, which in turn has an effective index of refraction  $n$  less than that of the bottom dielectric portion B (see Fig. 2). In other words,  $n_T < n_M < n_B$ , where  $n_T$  is the effective index of refraction of the top dielectric portion T,  $n_M$  is the effective index of refraction of the middle dielectric portion M, and  $n_B$  is the effective index of refraction of the bottom dielectric portion B (the "effective" index may be calculated as a weighted average of the portion, or by any other suitable technique/method). As shown in Fig. 2, each of the top, middle and bottom dielectric portions T, M and B, respectively, can include a plurality of different dielectric layers, although in alternative embodiments any or all of these portions need only include a single dielectric layer.

**[0031]** By gradually decreasing the respective effective indices of refraction "n" from the innermost or bottom dielectric portion B, to the middle dielectric portion M, and on to the top dielectric portion T toward the air, the anti-reflection system of Fig. 2 enables increased visible transmission and/or reduced visible reflection to be achieved. Surprisingly, as will be shown below in the Examples of this embodiment, the anti-reflection system also enables fairly neutral color of the coated article. Moreover, in certain example embodiments of this invention,  $n_T \leq 2.0$ . The silicon oxide layers herein may be from about 10-700 Å thick in certain example embodiments of this invention, more preferably from 20-600 Å thick, and most preferably from 50-500 Å thick. Upper tin oxide layers herein (i.e., in top portion T above the top IR reflecting layer) may be from about 10-700 Å thick in certain example embodiments of this invention, more preferably from 20-600 Å thick, and most preferably from 40-400 Å thick. Upper titanium oxide layers herein (i.e., in top portion T above the top IR reflecting layer) may be from about 10-500 Å thick in certain example embodiments of this invention, more preferably from 40-300 Å thick. Middle titanium oxide layers herein (i.e., in middle portion M between the IR reflecting layers) may be from about 10-900 Å thick in certain example embodiments of this invention, more preferably from 50-700 Å thick. Bottom titanium oxide layers herein (i.e., in bottom portion B below the lower IR reflecting layer) may have thicknesses as discussed in 09/794,224.



[0032] As with all embodiments herein, the illustrated layers are preferably deposited/formed via sputtering (see the Examples in the 09/794,224 application), although other deposition techniques may certainly be used in alternative embodiments of this invention.

#### EXAMPLE(S) OF FIG. 2 EMBODIMENT

[0033] The Tables below illustrate Example 1 of the Fig. 2 embodiment, which are to be compared to a Comparative Example(s) (CE) similar to Fig. 1 of the instant application. Thus, the CE relates to a coating that is similar to that illustrated in the 09/794,224 application. For the simulation examples herein, the following indices of refraction were assumed at 550 nm: for glass,  $n=1.51$ ; for  $\text{Si}_3\text{N}_4$ ,  $n=2.0$ ; for  $\text{SiO}_x\text{N}_y$ ,  $n=1.72$ ; for  $\text{SiO}_2$ ,  $n=1.45$ ; for  $\text{SnO}_2$ ,  $n=2.0$ ; for  $\text{Nb}_2\text{O}_5$ ,  $n=2.33$ ; for  $\text{SiZrN}_x$ ,  $n=2.32$ ; and for  $\text{TiO}_2$ ,  $n=2.57$  (note: approximately stoichiometric titanium oxide was assumed in all simulations herein). The thicknesses for each of the layers in the First Table below are in angstroms ( $\text{\AA}$ ). The Second Table below sets forth the optical characteristics (e.g., visible transmission, color, etc.) for the Example(s) and CE based upon being annealed and in monolithic form. All glass substrates were the same with respect to thickness and color. The total dielectric parameter simply adds up the total thickness of all dielectric layers in the coating (i.e., does not include Ag or  $\text{NiCrO}_x$  layers).

[0034] It is noted that the examples and comparative examples (CEs) herein utilized more oxidized  $\text{NiCrO}_x$  layers than did the examples in the 09/794,224 application (this explains why the comparative examples herein, in monolithic non-heat-treated form, have higher visible transmission than monolithic non-heat treated products in the 09/794,224). However, this distinction is not relevant because all  $\text{NiCrO}_x$  layers herein were assumed to have the same amount of oxidation, so that the comparisons herein between the CEs and the Examples are consistent. It is also noted that the indices for all Ag and  $\text{NiCrO}_x$  layers are assumed to be the same for all such layers in the Examples and the CEs herein. For optical performance (e.g., visible transmission), each of the parameters in the tables below is with respect to Ill. C, 2 degree observer. No example herein was considered heat treated.

FIRST TABLE: LAYER STRUCTURE – thicknesses (Fig. 2 embodiment)

	CE	Ex. 1
Glass		
TiO <sub>2</sub>	125Å	285Å
Si <sub>3</sub> N <sub>4</sub>	165Å	0Å
NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	16Å
TiO <sub>2</sub>	0Å	615Å
SnO <sub>2</sub>	672Å	7Å
Si <sub>3</sub> N <sub>4</sub>	165Å	0Å
NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	16Å
TiO <sub>2</sub>	0Å	230Å
SnO <sub>2</sub>	227Å	45Å
Si <sub>3</sub> N <sub>4</sub>	252Å	0Å
SiO <sub>x</sub> N <sub>y</sub>	0Å	0Å
SiO <sub>2</sub>	0Å	380Å
Total diel:	1606Å	1562 Å

SECOND TABLE: OPTICAL PERFORMANCE (Fig. 2 embodiment; monolithic)

	T <sub>vis</sub>	a* <sub>t</sub>	b* <sub>t</sub>	R <sub>glass side (g)</sub>	a* <sub>g</sub>	b* <sub>g</sub>	R <sub>film side (f)</sub>	a* <sub>f</sub>	b* <sub>f</sub>
Ex. 1:	79.2%	-0.7	-0.8	4.7%	4.6	-4.9	3.8%	3.3	-2.3
CE:	75.5%	-2.1	0.2	5.9%	9.2	-10.6	5.2%	3.2	-1.0

[0035] It can be seen from the Tables above regarding the Fig. 2 embodiment of this invention, that the anti-reflection system of the instant invention enables not only better visible transmission characteristics (i.e., increased transmission  $T_{vis}$  %, Ill. C, 2 deg.), but also reduced reflection (e.g., lower glass side reflection and/or film side reflection). Moreover, fairly neutral transmissive color is also provided. Surprisingly, it can be seen that the Fig. 2 embodiment provides more neutral color (e.g., transmissive  $a^*$  and glass side reflective) than does the CE. In particular, Example 1 (see Fig. 2) had better visible transmission (higher  $T_{vis}$ ) and better glass and/or film side reflection (lower  $R_g$  and/or  $R_f$ ), and more neutral transmissive  $a^*$ , glass side reflective  $a^*$ ,  $b^*$  color than the Comparative Example (CE).

[0036] Figure 3 is a cross sectional view of a coated article according to another embodiment of this invention. The Fig. 3 embodiment differs from the Fig. 2 embodiment in that the top dielectric portion T includes only a silicon nitride layer (stoichiometric  $Si_3N_4$ , or alternative a non-stoichiometric type of silicon nitride such as but not limited to a Si-rich type). The Fig. 3 embodiment differs from Fig. 1 (i.e., from the CE) in that (a) the bottom silicon nitride layer from Fig. 1 has been removed, (b) a titanium oxide layer has been added in the middle portion M, (c) the middle silicon nitride layer from Fig. 1 has been removed, and (d) the top tin oxide layer from Fig. 1 has been removed. As with all other embodiments herein which use titanium oxide, unless otherwise stated, the titanium oxide may be stoichiometric  $TiO_2$ , or alternatively a non-stoichiometric form such as  $TiO_{1.50-1.99}$ . Likewise, as with all other embodiments herein which use silicon nitride, unless otherwise stated the silicon nitride may be stoichiometric ( $Si_3N_4$ ) or non-stoichiometric (e.g., Si-rich). The coated article of Fig. 3 includes from the glass substrate outwardly (all indices  $n$  at 550 nm):

glass ( $n=1.51$ )

titanium oxide (e.g.,  $TiO_2$ ) ( $n=2.1$  to  $2.7$ , preferably  $n=2.4$  to  $2.65$ )

nickel-chromium-oxide ( $NiCrO_x$ )

silver (Ag)

nickel-chromium-oxide ( $NiCrO_x$ )

titanium oxide (e.g.,  $TiO_2$ ) ( $n=2.1$  to  $2.7$ , preferably  $n=2.4$  to  $2.65$ )

tin oxide (e.g.,  $\text{SnO}_2$ ) ( $n=1.8$  to  $2.2$ , preferably  $n=2.0$ )

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

silver ( $\text{Ag}$ )

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

silicon nitride (e.g.,  $\text{Si}_3\text{N}_4$ ) ( $n=1.8$  to  $2.0$ , preferably  $n=2.0$ )

air ( $n=1.0$ )

**[0037]** By using the silicon nitride over the top contact layer in the top dielectric portion T, and the higher index titanium oxide in the middle M and bottom B portion (diluted with the tin oxide in the middle portion M), the layer system can be characterized by the top dielectric portion T having an effective index of refraction  $n$  less than that of middle dielectric portion M, which in turn has an effective index of refraction  $n$  less than that of the bottom dielectric portion B. In other words,  $n_T < n_M < n_B$ , where  $n_T$  is the effective index of refraction of the top dielectric portion T (i.e., of the silicon nitride layer in this embodiment),  $n_M$  is the effective index of refraction of the middle dielectric portion M (i.e., of the tin oxide and titanium oxide layers in this embodiment), and  $n_B$  is the effective index of refraction of the bottom dielectric portion B (i.e., of the titanium oxide layer in this embodiment). Each of the top, middle and bottom dielectric portions T, M and B, respectively, can include a plurality of different dielectric layers, although in alternative embodiments any or all of these portions need only include a single dielectric layer (e.g. portions B and T in this Fig. 3 embodiment). By gradually decreasing the respective effective indices of refraction "n" from the innermost or bottom dielectric portion B, to the middle dielectric portion M, and on to the top dielectric portion T toward the air, the anti-reflection system of Fig. 3 enables increased visible transmission to be achieved. The term "effective" means the overall effective index  $n$  in a particular portion B, T or M, regardless of how many dielectric layers are provided therein. The anti-reflection system may also enable fairly neutral color of the coated article in certain example embodiments. The silicon nitride layer in portion T may be from about 10-900 Å thick in certain example embodiments of this invention, more preferably from 20-600 Å thick, and most preferably from 50-500 Å thick.

# EXAMPLE(S) OF FIG. 3 EMBODIMENT

[0038] The Tables below illustrate Example 1 of the Fig. 3 embodiment, compared to a Comparative Example(s) (CE) similar to Fig. 1 of the instant application. Thus, the CE relates to a coating that is similar to that illustrated in the 09/794,224 application. The thicknesses for each of the layers in the First Table below are in angstroms (Å). The Second Table below sets forth the optical characteristics (e.g., visible transmission, color, etc.) for Example 1 and the CE based upon being annealed and in monolithic form.

FIRST TABLE: LAYER STRUCTURE – thicknesses (Fig. 3 embodiment)

	CE	Ex. 1
Glass		
TiO <sub>2</sub>	125Å	276Å
Si <sub>3</sub> N <sub>4</sub>	165Å	0Å
NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	16Å
TiO <sub>2</sub>	0Å	496Å
SnO <sub>2</sub>	672Å	112Å
Si <sub>3</sub> N <sub>4</sub>	165Å	0Å
NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	16Å
TiO <sub>2</sub>	0Å	0Å
SnO <sub>2</sub>	227Å	0Å
Si <sub>3</sub> N <sub>4</sub>	252Å	420Å

SiO <sub>x</sub> N <sub>y</sub>	0Å	0Å
SiO <sub>2</sub>	0Å	0Å
Total diel:	1606Å	1304 Å

SECOND TABLE: OPTICAL PERFORMANCE (Fig. 3 embodiment; monolithic)

	T <sub>vis</sub>	a* <sub>t</sub>	b* <sub>t</sub>	R <sub>glass side (g)</sub>	a* <sub>g</sub>	b* <sub>g</sub>	R <sub>film side (f)</sub>	a* <sub>f</sub>	b* <sub>f</sub>
Ex. 1:	78.8%	-0.8	-0.4	4.5%	3.9	-5.0	3.3%	3.3	-2.3
CE:	75.5%	-2.1	0.2	5.9%	9.2	-10.6	5.2%	3.2	-1.0

**[0039]** It can be seen from the Tables above regarding the Fig. 3 embodiment of this invention, that the anti-reflection system of the instant invention enables not only better visible transmission characteristics (i.e., increased visible transmission T<sub>vis</sub> %), but also reduced reflection (e.g., lower glass side reflection and/or film side visible reflection). In particular, Example 1 (see Fig. 3) had better visible transmission (higher T<sub>vis</sub>) and better glass and/or film side reflection (lower R<sub>g</sub> and/or R<sub>f</sub>) than the Comparative Example (CE – see Fig. 1). Surprisingly, the Example 1 of this embodiment also had more neutral color than the CE with respect to transmissive a\*, and particularly with respect to glass side reflective a\*, b\*.

**[0040]** Figure 4 is a cross sectional view of a coated article according to another embodiment of this invention. The Fig. 4 embodiment differs from the Fig. 2 embodiment in that an additional silicon nitride layer has been added in the bottom dielectric portion B between the lower contact layer and the titanium oxide layer. The term "between" as used herein to state that a layer(s) is "between" layers x and y does not mean that the layer(s) contacts layer x or layer y; it merely means that the layer(s) is between the layers x and y regardless of whether other layer(s) are also between layers x and y. The coated article of Fig. 4 includes from the glass substrate outwardly (all indices n at 550 nm):

glass (n=1.51)

titanium oxide (e.g., TiO<sub>2</sub>) (n=2.1 to 2.7, preferably n=2.4 to 2.65)

silicon nitride (e.g., Si<sub>3</sub>N<sub>4</sub>) (n=1.8 to 2.0, preferably n=2.0)

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

silver (Ag)

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

titanium oxide (e.g.,  $\text{TiO}_2$ ) ( $n=2.1$  to  $2.7$ , preferably  $n=2.4$  to  $2.65$ )

tin oxide (e.g.,  $\text{SnO}_2$ ) ( $n=1.8$  to  $2.2$ , preferably  $n=2.0$ )

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

silver (Ag)

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

titanium oxide (e.g.,  $\text{TiO}_2$ ) ( $n=2.1$  to  $2.7$ , preferably  $n=2.4$  to  $2.65$ )

tin oxide (e.g.,  $\text{SnO}_2$ ) ( $n=1.8$  to  $2.2$ , preferably  $n=2.0$ )

silicon oxide (e.g.,  $\text{SiO}_2$ ) ( $n=1.4$  to  $1.7$ , preferably  $n=1.45$ )

air ( $n=1.0$ )

**[0041]** By using the silicon oxide, tin oxide, titanium oxide and silicon nitride dielectric layers as shown in this embodiment, the layer system can be characterized by the top dielectric portion T having an effective index of refraction  $n$  less than that of middle dielectric portion M, which in turn has an effective index of refraction  $n$  less than that of the bottom dielectric portion B. In other words,  $n_T < n_M < n_B$ , where  $n_T$  is the effective index of refraction of the top dielectric portion T,  $n_M$  is the effective index of refraction of the middle dielectric portion M, and  $n_B$  is the effective index of refraction of the bottom dielectric portion B. Each of the top, middle and bottom dielectric portions T, M and B, respectively, can include a plurality of different dielectric layers, although in alternative embodiments any or all of these portions need only include a single dielectric layer. By gradually decreasing the respective effective indices of refraction " $n$ " from the innermost or bottom dielectric portion B, to the middle dielectric portion M, and on to the top dielectric portion T toward the air, the anti-reflection system of this embodiment enables increased visible transmission to be achieved. Surprisingly, the anti-reflection system may also enable fairly neutral color of the coated article in certain example embodiments.

# EXAMPLE(S) OF FIG. 4 EMBODIMENT

**[0042]** The Tables below illustrate Examples 1-4 of the Fig. 4 embodiment, compared to a Comparative Example(s) (CE) similar to Fig. 1 of the instant application. Thus, the CE relates to a coating that is similar to that illustrated in the 09/794,224 application. The thicknesses for each of the layers in the First Table below are in angstroms (Å). The Second Table below sets forth the optical characteristics (e.g., visible transmission, color, etc.) for Examples 1-4 and the CE based upon being annealed and in monolithic form.

FIRST TABLE: LAYER STRUCTURE – thicknesses (Fig. 4 embodiment)

	CE	Ex. 1	Ex. 2	Ex. 3	Ex. 4
Glass					
TiO <sub>2</sub>	125Å	125Å	269Å	230 Å	125 Å
Si <sub>3</sub> N <sub>4</sub>	165Å	199Å	54Å	60 Å	198 Å
NiCrO <sub>x</sub>	18Å	18Å	18Å	18 Å	18 Å
Ag	98Å	98Å	98 Å	98 Å	98 Å
NiCrO <sub>x</sub>	16Å	16Å	16 Å	16 Å	16 Å
TiO <sub>2</sub>	0Å	481Å	219 Å	120 Å	120 Å
SnO <sub>2</sub>	672Å	113Å	710 Å	837 Å	782 Å
Si <sub>3</sub> N <sub>4</sub>	165Å	0Å	0 Å	0 Å	0 Å
NiCrO <sub>x</sub>	18Å	18Å	18 Å	18 Å	18 Å
Ag	98Å	98Å	98 Å	98 Å	98 Å
NiCrO <sub>x</sub>	16Å	16Å	16 Å	16 Å	16 Å
TiO <sub>2</sub>	0Å	210Å	181 Å	190 Å	190 Å
SnO <sub>2</sub>	227Å	34Å	32 Å	32 Å	10 Å
Si <sub>3</sub> N <sub>4</sub>	252Å	0Å	0 Å	0 Å	0 Å



SiO <sub>x</sub> N <sub>y</sub>	0 Å	0 Å	0 Å	0 Å	0 Å
SiO <sub>2</sub>	0 Å	404 Å	334 Å	373 Å	435 Å
Total diel:	1606 Å	1566 Å	1799 Å	1842 Å	1860 Å

SECOND TABLE: OPTICAL PERFORMANCE (Fig. 4 embodiment; monolithic)

	T <sub>vis</sub>	a* <sub>t</sub>	b* <sub>t</sub>	R <sub>glass side (g)</sub>	a* <sub>g</sub>	b* <sub>g</sub>	R <sub>film side (f)</sub>	a* <sub>f</sub>	b* <sub>f</sub>
Ex. 1:	78.3%	-1.5	-0.1	5.0%	9.1	-7.1	3.9%	3.8	-2.4
Ex. 2:	78.2%	-1.7	0.9	4.5%	7.6	-11.9	4.1%	0.6	-3.5
Ex. 3:	78.1%	-1.6	0.6	4.5%	5.1	-9.4	4.0%	2.3	-3.0
Ex. 4:	77.8%	-2.1	1.2	4.5%	9.2	-12.4	3.9%	3.9	-2.4
CE:	75.5%	-2.1	0.2	5.9%	9.2	-10.6	5.2%	3.2	-1.0

**[0043]** It can be seen from the Tables above regarding the Fig. 4 embodiment of this invention, that the anti-reflection system of the instant invention enables not only better visible transmission characteristics (i.e., increased visible transmission T<sub>vis</sub> %), but also reduced reflection (e.g., lower glass side reflection and/or film side visible reflection). In particular, Examples 1-4 (see Fig. 4) had better visible transmission (higher T<sub>vis</sub>) and better glass and/or film side reflection (lower R<sub>g</sub> and/or R<sub>f</sub>) than the Comparative Example (CE – see Fig. 1). Fairly neutral color was also achieved in the Example(s).

**[0044]** Figure 5 is a cross sectional view of a coated article according to another embodiment of this invention. The Fig. 5 embodiment differs from the Fig. 3 embodiment in that an additional silicon nitride layer has been added in the bottom dielectric portion B between the lower contact layer and the titanium oxide layer, and a silicon oxide layer has been added over the silicon nitride layer in the top dielectric portion T. The coated article of Fig. 5 includes from the glass substrate outwardly (all indices n at 550 nm):

glass (n=1.51)

titanium oxide (e.g., TiO<sub>2</sub>) (n=2.1 to 2.7, preferably n=2.4 to 2.65)

silicon nitride (e.g.,  $\text{Si}_3\text{N}_4$ ) ( $n=1.8$  to  $2.0$ , preferably  $n=2.0$ )

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

silver (Ag)

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

titanium oxide (e.g.,  $\text{TiO}_2$ ) ( $n=2.1$  to  $2.7$ , preferably  $n=2.4$  to  $2.65$ )

tin oxide (e.g.,  $\text{SnO}_2$ ) ( $n=1.8$  to  $2.2$ , preferably  $n=2.0$ )

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

silver (Ag)

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

silicon nitride (e.g.,  $\text{Si}_3\text{N}_4$ ) ( $n=1.8$  to  $2.0$ , preferably  $n=2.0$ )

silicon oxide (e.g.,  $\text{SiO}_2$ ) ( $n=1.4$  to  $1.7$ , preferably  $n=1.45$ )

air ( $n=1.0$ )

**[0045]** By using the silicon oxide, tin oxide, titanium oxide and silicon nitride dielectric layers as shown in this embodiment, the layer system can be characterized by the top dielectric portion T having an effective index of refraction  $n$  less than that of middle dielectric portion M, which in turn has an effective index of refraction  $n$  less than or equal to that of the bottom dielectric portion B. In other words,  $n_T < n_M \leq n_B$ , where  $n_T$  is the effective index of refraction of the top dielectric portion T,  $n_M$  is the effective index of refraction of the middle dielectric portion M, and  $n_B$  is the effective index of refraction of the bottom dielectric portion B. Each of the top, middle and bottom dielectric portions T, M and B, respectively, can include a plurality of different dielectric layers, although in alternative embodiments any or all of these portions need only include a single dielectric layer. By gradually decreasing the respective effective indices of refraction "n" from the innermost or bottom dielectric portion B, to the middle dielectric portion M, and on to the top dielectric portion T toward the air, the anti-reflection system of this embodiment enables increased visible transmission to be achieved. Surprisingly, the anti-reflection system may also enable fairly neutral color of the coated article in certain example embodiments.

# EXAMPLE(S) OF FIG. 5 EMBODIMENT

[0046] The Tables below illustrate Example 1 of the Fig. 5 embodiment, compared to a Comparative Example(s) (CE) similar to Fig. 1 of the instant application. The CE relates to a coating that is similar to that illustrated in the 09/794,224 application. The thicknesses for each of the layers in the First Table below are in angstroms (Å). The Second Table below sets forth the optical characteristics (e.g., visible transmission, color, etc.) for Example 1 and the CE based upon being annealed and in monolithic form.

FIRST TABLE: LAYER STRUCTURE – thicknesses (Fig. 5 embodiment)

	CE	Ex. 1
Glass		
TiO <sub>2</sub>	125Å	125Å
Si <sub>3</sub> N <sub>4</sub>	165Å	196Å
NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	16Å
TiO <sub>2</sub>	0Å	488Å
SnO <sub>2</sub>	672Å	91Å
Si <sub>3</sub> N <sub>4</sub>	165Å	0Å
NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	16Å
TiO <sub>2</sub>	0Å	0Å
SnO <sub>2</sub>	227Å	0Å
Si <sub>3</sub> N <sub>4</sub>	252Å	379Å
SiO <sub>x</sub> N <sub>y</sub>	0Å	0Å

SiO<sub>2</sub>            0Å      147Å  
 Total diel: 1606Å    1426 Å

SECOND TABLE: OPTICAL PERFORMANCE (Fig. 5 embodiment; monolithic)

	T <sub>vis</sub>	a* <sub>t</sub>	b* <sub>t</sub>	R <sub>glass side (g)</sub>	a* <sub>g</sub>	b* <sub>g</sub>	R <sub>film side (f)</sub>	a* <sub>f</sub>	b* <sub>f</sub>
Ex. 1:	78.1%	-1.5	0.0	5.0%	8.5	-6.7	3.8%	3.4	-2.5
CE:	75.5%	-2.1	0.2	5.9%	9.2	-10.6	5.2%	3.2	-1.0

[0047]            It can be seen from the Tables above regarding the Fig. 5 embodiment of this invention, that the anti-reflection system of the instant invention enables not only better visible transmission characteristics (i.e., increased visible transmission T<sub>vis</sub> %), but also reduced reflection (e.g., lower glass side reflection and/or film side visible reflection). In particular, Example 1 (see Fig. 5) had better visible transmission (higher T<sub>vis</sub>) and better glass and/or film side reflection (lower R<sub>g</sub> and/or R<sub>f</sub>) than the Comparative Example (CE – see Fig. 1). Surprisingly, Example 1 also had more neutral transmissive and glass side reflective color than the CE.

[0048]            Figure 6 is a cross sectional view of a coated article according to another embodiment of this invention. The Fig. 6 embodiment differs from the Fig. 2 embodiment in that the upper tin oxide layer in the portion T has been removed from the Fig. 2 embodiment and an additional silicon nitride layer has been added in the bottom dielectric portion B between the lower contact layer and the titanium oxide layer. The coated article of Fig. 6 includes from the glass substrate outwardly (all indices n at 550 nm):

glass (n=1.51)  
 titanium oxide (e.g., TiO<sub>2</sub>) (n=2.1 to 2.7, preferably n=2.4 to 2.65)  
 silicon nitride (e.g., Si<sub>3</sub>N<sub>4</sub>) (n=1.8 to 2.0, preferably n=2.0)  
 nickel-chromium-oxide (NiCrO<sub>x</sub>)  
 silver (Ag)  
 nickel-chromium-oxide (NiCrO<sub>x</sub>)

titanium oxide (e.g.,  $\text{TiO}_2$ ) ( $n=2.1$  to  $2.7$ , preferably  $n=2.4$  to  $2.65$ )

tin oxide (e.g.,  $\text{SnO}_2$ ) ( $n=1.8$  to  $2.2$ , preferably  $n=2.0$ )

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

silver (Ag)

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

titanium oxide (e.g.,  $\text{TiO}_2$ ) ( $n=2.1$  to  $2.7$ , preferably  $n=2.4$  to  $2.65$ )

silicon oxide (e.g.,  $\text{SiO}_2$ ) ( $n=1.4$  to  $1.7$ , preferably  $n=1.45$ )

air ( $n=1.0$ )

**[0049]** By using the silicon oxide, tin oxide, titanium oxide and silicon nitride dielectric layers as shown in this embodiment, the layer system can be characterized by the top dielectric portion T having an effective index of refraction  $n$  less than that of middle dielectric portion M, which in turn has an effective index of refraction  $n$  less than or equal to that of the bottom dielectric portion B. In other words,  $n_T < n_M \leq n_B$ , where  $n_T$  is the effective index of refraction of the top dielectric portion T,  $n_M$  is the effective index of refraction of the middle dielectric portion M, and  $n_B$  is the effective index of refraction of the bottom dielectric portion B. Each of the top, middle and bottom dielectric portions T, M and B, respectively, can include a plurality of different dielectric layers, although in alternative embodiments any or all of these portions need only include a single dielectric layer. By gradually decreasing the respective effective indices of refraction "n" from the innermost or bottom dielectric portion B, to the middle dielectric portion M, and on to the top dielectric portion T toward the air, the anti-reflection system of this embodiment enables increased visible transmission to be achieved. Surprisingly, the anti-reflection system may also enable fairly neutral color of the coated article in certain example embodiments.

#### EXAMPLE(S) OF FIG. 6 EMBODIMENT

**[0050]** The Tables below illustrate Example 1 of the Fig. 6 embodiment, compared to a Comparative Example(s) (CE) similar to Fig. 1 of the instant application. The CE relates to a coating that is similar to that illustrated in the

09/794,224 application. The thicknesses for each of the layers in the First Table below are in angstroms (Å). The Second Table below sets forth the optical characteristics (e.g., visible transmission, color, etc.) for Example 1 and the CE based upon being annealed and in monolithic form.

FIRST TABLE: LAYER STRUCTURE – thicknesses (Fig. 6 embodiment)

	CE	Ex. 1
Glass		
TiO <sub>2</sub>	125Å	125Å
Si <sub>3</sub> N <sub>4</sub>	165Å	201Å
NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	16Å
TiO <sub>2</sub>	0Å	477Å
SnO <sub>2</sub>	672Å	71Å
Si <sub>3</sub> N <sub>4</sub>	165Å	0Å
NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	16Å
TiO <sub>2</sub>	0Å	195Å
SnO <sub>2</sub>	227Å	0Å
Si <sub>3</sub> N <sub>4</sub>	252Å	0Å
SiO <sub>x</sub> N <sub>y</sub>	0Å	0Å
SiO <sub>2</sub>	0Å	509Å
Total diel:	1606Å	1578 Å

SECOND TABLE: OPTICAL PERFORMANCE (Fig. 6 embodiment; monolithic)

	$T_{vis}$	$a^*_t$	$b^*_t$	$R_{glass\ side\ (g)}$	$a^*_g$	$b^*_g$	$R_{film\ side\ (f)}$	$a^*_f$	$b^*_f$
Ex. 1:	78.1%	-1.1	-0.3	4.9%	4.7	-2.6	3.4%	2.0	-4.7
CE:	75.5%	-2.1	0.2	5.9%	9.2	-10.6	5.2%	3.2	-1.0

**[0051]** It can be seen from the Tables above regarding the Fig. 6 embodiment of this invention, that the anti-reflection system of the instant invention enables not only better visible transmission characteristics (i.e., increased visible transmission  $T_{vis}$  %), but also reduced reflection (e.g., lower glass side reflection and/or film side visible reflection). In particular, Example 1 (see Fig. 6) had better visible transmission (higher  $T_{vis}$ ) and better glass and/or film side reflection (lower  $R_g$  and/or  $R_f$ ) than the Comparative Example (CE – see Fig. 1). Surprisingly, Example 1 also had more neutral transmissive and glass side reflective color than the CE.

**[0052]** Figure 7 is a cross sectional view of a coated article according to another embodiment of this invention. The Fig. 7 embodiment differs from the Fig. 2 embodiment in that the upper titanium oxide layer from the Fig. 2 embodiment in portion T has been removed, and an additional silicon nitride layer has been added in Fig. 7 in the bottom dielectric portion B between the lower contact layer and the titanium oxide layer. The coated article of Fig. 7 includes from the glass substrate outwardly (all indices  $n$  at 550 nm):

glass ( $n=1.51$ )

titanium oxide (e.g.,  $TiO_2$ ) ( $n=2.1$  to  $2.7$ , preferably  $n=2.4$  to  $2.65$ )

silicon nitride (e.g.,  $Si_3N_4$ ) ( $n=1.8$  to  $2.0$ , preferably  $n=2.0$ )

nickel-chromium-oxide ( $NiCrO_x$ )

silver (Ag)

nickel-chromium-oxide ( $NiCrO_x$ )

titanium oxide (e.g.,  $TiO_2$ ) ( $n=2.1$  to  $2.7$ , preferably  $n=2.4$  to  $2.65$ )

tin oxide (e.g.,  $SnO_2$ ) ( $n=1.8$  to  $2.2$ , preferably  $n=2.0$ )

nickel-chromium-oxide ( $NiCrO_x$ )

silver (Ag)

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

tin oxide (e.g.,  $\text{SnO}_2$ ) ( $n=1.8$  to  $2.2$ , preferably  $n=2.0$ )

silicon oxide (e.g.,  $\text{SiO}_2$ ) ( $n=1.4$  to  $1.7$ , preferably  $n=1.45$ )

air ( $n=1.0$ )

**[0053]** By using the silicon oxide, tin oxide, titanium oxide and silicon nitride dielectric layers as shown in this embodiment, the layer system can be characterized by the top dielectric portion T having an effective index of refraction  $n$  less than that of middle dielectric portion M, which in turn has an effective index of refraction  $n$  less than or equal to that of the bottom dielectric portion B. In other words,  $n_T < n_M \leq n_B$ , where  $n_T$  is the effective index of refraction of the top dielectric portion T,  $n_M$  is the effective index of refraction of the middle dielectric portion M, and  $n_B$  is the effective index of refraction of the bottom dielectric portion B. Each of the top, middle and bottom dielectric portions T, M and B, respectively, can include a plurality of different dielectric layers, although in alternative embodiments any or all of these portions need only include a single dielectric layer. By gradually decreasing the respective effective indices of refraction " $n$ " from the innermost or bottom dielectric portion B, to the middle dielectric portion M, and on to the top dielectric portion T toward the air, the anti-reflection system of this embodiment enables increased visible transmission to be achieved. Surprisingly, the anti-reflection system may also enable fairly neutral color of the coated article in certain example embodiments.

#### EXAMPLE(S) OF FIG. 7 EMBODIMENT

**[0054]** The Tables below illustrate Example 1 of the Fig. 7 embodiment, compared to a Comparative Example(s) (CE) similar to Fig. 1 of the instant application. The CE relates to a coating that is similar to that illustrated in the 09/794,224 application. The thicknesses for each of the layers in the First Table below are in angstroms ( $\text{\AA}$ ). The Second Table below sets forth the optical characteristics (e.g., visible transmission, color, etc.) for Example 1 and the CE based upon being annealed and in monolithic form.



FIRST TABLE: LAYER STRUCTURE – thicknesses (Fig. 7 embodiment)

	CE	Ex. 1
Glass		
TiO <sub>2</sub>	125Å	125Å
Si <sub>3</sub> N <sub>4</sub>	165Å	220Å
NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	16Å
TiO <sub>2</sub>	0Å	171Å
SnO <sub>2</sub>	672Å	690Å
Si <sub>3</sub> N <sub>4</sub>	165Å	0Å
NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	16Å
TiO <sub>2</sub>	0Å	0Å
SnO <sub>2</sub>	227Å	307Å
Si <sub>3</sub> N <sub>4</sub>	252Å	0Å
SiO <sub>x</sub> N <sub>y</sub>	0Å	0Å
SiO <sub>2</sub>	0Å	222Å
Total diel:	1606Å	1735 Å

SECOND TABLE: OPTICAL PERFORMANCE (Fig. 7 embodiment; monolithic)

	T <sub>vis</sub>	a* <sub>t</sub>	b* <sub>t</sub>	R <sub>glass side (g)</sub>	a* <sub>g</sub>	b* <sub>g</sub>	R <sub>film side (f)</sub>	a* <sub>f</sub>	b* <sub>f</sub>
Ex. 1:	77.7%	-2.1	1.5	4.5%	10.0	-13.7	3.7%	3.0	-2.7
CE:	75.5%	-2.1	0.2	5.9%	9.2	-10.6	5.2%	3.2	-1.0

**[0055]** It can be seen from the Tables above regarding the Fig. 7 embodiment of this invention, that the anti-reflection system of the instant invention enables not only better visible transmission characteristics (i.e., increased visible transmission  $T_{vis}$  %), but also reduced reflection (e.g., lower glass side reflection and/or film side visible reflection). In particular, Example 1 (see Fig. 7) had better visible transmission (higher  $T_{vis}$ ) and better glass and/or film side reflection (lower  $R_g$  and/or  $R_f$ ) than the Comparative Example (CE – see Fig. 1). Surprisingly, Example 1 also had fairly neutral color.

**[0056]** Figure 8 is a cross sectional view of a coated article according to another embodiment of this invention. The Fig. 8 embodiment differs from the Fig. 4 embodiment in that the upper dielectric portion in the Fig. 8 embodiment includes a silicon oxynitride layer. The silicon oxynitride layer is beneficial in that its index of refraction  $n$  (at 550 nm) can be varied from 1.45 to 2.0, more preferably from 1.6 to 1.9, and most preferably from 1.65 to 1.85, in different embodiments of this invention. In this and all other silicon oxynitride inclusive embodiments herein, the silicon oxynitride layer may have a constant (or approximately constant, i.e., constant plus/minus about 5%) index of refraction  $n$  throughout its entire thickness in certain embodiments of this invention, but alternatively may be oxidation and/or nitride graded so as to have an index of refraction  $n$  which varies through the thickness of the layer (e.g., the index  $n$  may gradually decrease through the thickness of the silicon oxynitride layer moving toward the air). The coated article of Fig. 8 includes from the glass substrate outwardly (all indices  $n$  at 550 nm):

glass ( $n=1.51$ )

titanium oxide (e.g.,  $TiO_2$ ) ( $n=2.1$  to  $2.7$ , preferably  $n=2.4$  to  $2.65$ )

silicon nitride (e.g.,  $Si_3N_4$ ) ( $n=1.8$  to  $2.0$ , preferably  $n=2.0$ )

nickel-chromium-oxide ( $NiCrO_x$ )

silver (Ag)

nickel-chromium-oxide ( $NiCrO_x$ )

titanium oxide (e.g.,  $TiO_2$ ) ( $n=2.1$  to  $2.7$ , preferably  $n=2.4$  to  $2.65$ )

tin oxide (e.g.,  $\text{SnO}_2$ ) ( $n=1.8$  to  $2.2$ , preferably  $n=2.0$ )

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

silver (Ag)

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

silicon oxynitride (e.g.,  $\text{SiO}_x\text{N}_y$ ) ( $n=1.45$ - $2.0$ , preferably  $n=1.6$ - $1.9$ )

air ( $n=1.0$ )

**[0057]** By using the silicon oxynitride, tin oxide, titanium oxide and silicon nitride dielectric layers as shown in this embodiment, the layer system can be characterized by the top dielectric portion T having an effective index of refraction  $n$  (e.g.,  $n=1.72$  at  $550$  nm, as an example of an index  $n$  of silicon oxynitride) less than that of middle dielectric portion M, which in turn has an effective index of refraction  $n$  less than or equal to that of the bottom dielectric portion B. In other words,  $n_T < n_M \leq n_B$ , where  $n_T$  is the effective index of refraction of the top dielectric portion T,  $n_M$  is the effective index of refraction of the middle dielectric portion M, and  $n_B$  is the effective index of refraction of the bottom dielectric portion B. Each of the top, middle and bottom dielectric portions T, M and B, respectively, can include a plurality of different dielectric layers, although in alternative embodiments any or all of these portions need only include a single dielectric layer. By gradually decreasing the respective effective indices of refraction "n" from the innermost or bottom dielectric portion B, to the middle dielectric portion M, and on to the top dielectric portion T toward the air (not including the Ag or contact layers), the anti-reflection system of this embodiment enables increased visible transmission to be achieved. Surprisingly, the anti-reflection system may also enable fairly neutral color of the coated article in certain example embodiments.

#### EXAMPLE(S) OF FIG. 8 EMBODIMENT

**[0058]** The Tables below illustrate Example 1 of the Fig. 8 embodiment, compared to a Comparative Example(s) (CE) similar to Fig. 1 of the instant application. The CE relates to a coating that is similar to that illustrated in the 09/794,224 application. The thicknesses for each of the layers in the First Table

below are in angstroms (Å). The Second Table below sets forth the optical characteristics (e.g., visible transmission, color, etc.) for Example 1 and the CE based upon being annealed and in monolithic form.

FIRST TABLE: LAYER STRUCTURE – thicknesses (Fig. 8 embodiment)

	CE	Ex. 1
Glass		
TiO <sub>2</sub>	125Å	125Å
Si <sub>3</sub> N <sub>4</sub>	165Å	173Å
NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	16Å
TiO <sub>2</sub>	0Å	144Å
SnO <sub>2</sub>	672Å	665Å
Si <sub>3</sub> N <sub>4</sub>	165Å	0Å
NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	16Å
TiO <sub>2</sub>	0Å	0Å
SnO <sub>2</sub>	227Å	0Å
Si <sub>3</sub> N <sub>4</sub>	252Å	0Å
SiO <sub>x</sub> N <sub>y</sub>	0Å	503Å
SiO <sub>2</sub>	0Å	0Å
Total diel:	1606Å	1610 Å



nickel-chromium-oxide ( $\text{NiCrO}_x$ )

silver (Ag)

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

silicon zirconium nitride ( $\text{SiZrN}_x$ ) ( $n=2.2-2.45$ , preferably  $n=2.32$ )

tin oxide (e.g.,  $\text{SnO}_2$ ) ( $n=1.8$  to  $2.2$ , preferably  $n=2.0$ )

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

silver (Ag)

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

silicon zirconium nitride ( $\text{SiZrN}_x$ ) ( $n=2.2-2.45$ , preferably  $n=2.32$ )

tin oxide (e.g.,  $\text{SnO}_2$ ) ( $n=1.8$  to  $2.2$ , preferably  $n=2.0$ )

silicon oxide (e.g.,  $\text{SiO}_2$ ) ( $n=1.4$  to  $1.7$ , preferably  $n=1.45$ )

air ( $n=1.0$ )

**[0061]** By using the silicon zirconium nitride, silicon oxide, and tin oxide dielectric layers as shown in this embodiment, the layer system can be characterized by the top dielectric portion T having an effective index of refraction  $n$  less than that of middle dielectric portion M, which in turn has an effective index of refraction  $n$  less than that of the bottom dielectric portion B. In other words,  $n_T < n_M < n_B$ , where  $n_T$  is the effective index of refraction of the top dielectric portion T,  $n_M$  is the effective index of refraction of the middle dielectric portion M, and  $n_B$  is the effective index of refraction of the bottom dielectric portion B. Each of the top, middle and bottom dielectric portions T, M and B, respectively, can include a plurality of different dielectric layers, although in alternative embodiments any or all of these portions need only include a single dielectric layer. By gradually decreasing the respective effective indices of refraction " $n$ " from the innermost or bottom dielectric portion B, to the middle dielectric portion M, and on to the top dielectric portion T toward the air, the anti-reflection system of this embodiment enables increased visible transmission to be achieved. Surprisingly, the anti-reflection system may also enable fairly neutral color of the coated article in certain example embodiments.

## EXAMPLE(S) OF FIG. 9 EMBODIMENT

**[0062]** The Tables below illustrate Example 1 of the Fig. 9 embodiment, compared to a Comparative Example(s) (CE) similar to Fig. 1 of the instant application. The CE relates to a coating that is similar to that illustrated in the 09/794,224 application. The thicknesses for each of the layers in the First Table below are in angstroms (Å). The Second Table below sets forth the optical characteristics (e.g., visible transmission, color, etc.) for Example 1 and the CE based upon being annealed and in monolithic form.

FIRST TABLE: LAYER STRUCTURE – thicknesses (Fig. 9 embodiment)

	CE	Ex. 1
Glass		
SiZrN <sub>x</sub>	0Å	352Å
TiO <sub>2</sub>	125Å	0Å
Si <sub>3</sub> N <sub>4</sub>	165Å	0Å
NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	16Å
SiZrN <sub>x</sub>	0Å	232Å
SnO <sub>2</sub>	672Å	680Å
Si <sub>3</sub> N <sub>4</sub>	165Å	0Å
NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	16Å
SiZrN <sub>x</sub>	0Å	125Å
SnO <sub>2</sub>	227Å	143Å

Si <sub>3</sub> N <sub>4</sub>	252Å	0Å
SiO <sub>x</sub> N <sub>y</sub>	0Å	0Å
SiO <sub>2</sub>	0Å	327Å
Total diel:	1606Å	1859 Å

SECOND TABLE: OPTICAL PERFORMANCE (Fig. 9 embodiment; monolithic)

	T <sub>vis</sub>	a* <sub>t</sub>	b* <sub>t</sub>	R <sub>glass side (g)</sub>	a* <sub>g</sub>	b* <sub>g</sub>	R <sub>film side (f)</sub>	a* <sub>f</sub>	b* <sub>f</sub>
Ex. 1:	77.4%	-2.8	3.1	4.4%	7.8	-11.5	3.8%	3.3	-2.7
CE:	75.5%	-2.1	0.2	5.9%	9.2	-10.6	5.2%	3.2	-1.0

**[0063]** It can be seen from the Tables above regarding the Fig. 9 embodiment of this invention, that the anti-reflection system of the instant invention enables not only better visible transmission characteristics (i.e., increased visible transmission T<sub>vis</sub> %), but also reduced reflection (e.g., lower glass side reflection and/or film side visible reflection). In particular, Example 1 (see Fig. 9) had better visible transmission (higher T<sub>vis</sub>) and better glass and/or film side reflection (lower R<sub>g</sub> and/or R<sub>f</sub>) than the Comparative Example (CE – see Fig. 1). Surprisingly, Example 1 also had fairly neutral color.

**[0064]** Figure 10 is a cross sectional view of a coated article according to another embodiment of this invention. The Fig. 10 embodiment differs from the Fig. 9 embodiment in that the upper silicon oxide and SiZrN inclusive layers in the top dielectric portion T have been removed. It is noted that the silicon zirconium nitride inclusive layers may be stoichiometric or non-stoichiometric in different embodiments of this invention. Moreover, one or more of the silicon zirconium nitride (SiZrN) layers may be oxidized, and/or may be replaced with layer(s) comprising niobium oxide (e.g., Nb<sub>2</sub>O<sub>5</sub> or any other suitable form). The coated article of Fig. 10 includes from the glass substrate outwardly (all indices n at 550 nm):

glass (n=1.51)

silicon zirconium nitride (SiZrN<sub>x</sub>) (n=2.2-2.45, preferably n=2.32)



nickel-chromium-oxide ( $\text{NiCrO}_x$ )

silver (Ag)

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

silicon zirconium nitride ( $\text{SiZrN}_x$ ) ( $n=2.2-2.45$ , preferably  $n=2.32$ )

tin oxide (e.g.,  $\text{SnO}_2$ ) ( $n=1.8$  to  $2.2$ , preferably  $n=2.0$ )

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

silver (Ag)

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

tin oxide (e.g.,  $\text{SnO}_2$ ) ( $n=1.8$  to  $2.2$ , preferably  $n=2.0$ )

air ( $n=1.0$ )

**[0065]** By using the silicon zirconium nitride, silicon oxide, and tin oxide dielectric layers as shown in this embodiment, the layer system can be characterized by the top dielectric portion T having an effective index of refraction  $n$  less than that of middle dielectric portion M, which in turn has an effective index of refraction  $n$  less than that of the bottom dielectric portion B. In other words,  $n_T < n_M < n_B$ , where  $n_T$  is the effective index of refraction of the top dielectric portion T,  $n_M$  is the effective index of refraction of the middle dielectric portion M, and  $n_B$  is the effective index of refraction of the bottom dielectric portion B. Each of the top, middle and bottom dielectric portions T, M and B, respectively, can include a plurality of different dielectric layers, although in alternative embodiments any or all of these portions need only include a single dielectric layer. By gradually decreasing the respective effective indices of refraction " $n$ " from the innermost or bottom dielectric portion B, to the middle dielectric portion M, and on to the top dielectric portion T toward the air, the anti-reflection system of this embodiment enables increased visible transmission to be achieved. Surprisingly, the anti-reflection system may also enable fairly neutral color of the coated article in certain example embodiments.

# EXAMPLE(S) OF FIG. 10 EMBODIMENT

**[0066]** The Tables below illustrate Example 1 of the Fig. 10 embodiment, compared to a Comparative Example(s) (CE) similar to Fig. 1 of the instant application. The CE relates to a coating that is similar to that illustrated in the 09/794,224 application. The thicknesses for each of the layers in the First Table below are in angstroms (Å). The Second Table below sets forth the optical characteristics (e.g., visible transmission, color, etc.) for Example 1 and the CE based upon being annealed and in monolithic form.

FIRST TABLE: LAYER STRUCTURE – thicknesses (Fig. 10 embodiment)

	CE	Ex. 1
Glass		
SiZrN <sub>x</sub>	0Å	360Å
TiO <sub>2</sub>	125Å	0Å
Si <sub>3</sub> N <sub>4</sub>	165Å	0Å
NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	16Å
SiZrN <sub>x</sub>	0Å	240Å
SnO <sub>2</sub>	672Å	667Å
Si <sub>3</sub> N <sub>4</sub>	165Å	0Å
NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	16Å
SiZrN <sub>x</sub>	0Å	0Å
SnO <sub>2</sub>	227Å	399Å

Si <sub>3</sub> N <sub>4</sub>	252Å	0Å
SiO <sub>x</sub> N <sub>y</sub>	0Å	0Å
SiO <sub>2</sub>	0Å	0Å
Total diel:	1606Å	1666 Å

SECOND TABLE: OPTICAL PERFORMANCE (Fig. 10 embodiment; monolithic)

	T <sub>vis</sub>	a* <sub>t</sub>	b* <sub>t</sub>	R <sub>glass side (g)</sub>	a* <sub>g</sub>	b* <sub>g</sub>	R <sub>film side (f)</sub>	a* <sub>f</sub>	b* <sub>f</sub>
Ex. 1:	77.3%	-2.9	3.8	4.5%	9.2	-12.6	4.1%	3.2	-2.9
CE:	75.5%	-2.1	0.2	5.9%	9.2	-10.6	5.2%	3.2	-1.0

**[0067]** It can be seen from the Tables above regarding the Fig. 10 embodiment of this invention, that the anti-reflection system of the instant invention enables not only better visible transmission characteristics (i.e., increased visible transmission T<sub>vis</sub> %), but also reduced reflection (e.g., lower glass side reflection and/or film side visible reflection). In particular, Example 1 (see Fig. 10) had better visible transmission (higher T<sub>vis</sub>) and better glass and/or film side reflection (lower R<sub>g</sub> and/or R<sub>f</sub>) than the Comparative Example (CE – see Fig. 1). Surprisingly, Example 1 also had fairly neutral transmissive color.

**[0068]** Figure 11 is a cross sectional view of a coated article according to another embodiment of this invention. The Fig. 11 embodiment differs from the Fig. 10 embodiment in that the upper and middle tin oxide layers from Fig. 10 are replaced with respective layers of or including silicon nitride (stoichiometric or non-stoichiometric). It is noted that the silicon zirconium nitride inclusive layers may be stoichiometric or non-stoichiometric in different embodiments of this invention. Moreover, one or more of the silicon zirconium nitride (SiZrN) layers may be oxidized, and/or may be replaced with layer(s) comprising niobium oxide (e.g., Nb<sub>2</sub>O<sub>5</sub> or any other suitable form). The coated article of Fig. 11 includes from the glass substrate outwardly (all indices n at 550 nm):

glass (n=1.51)

silicon zirconium nitride (SiZrN<sub>x</sub>) (n=2.2-2.45, preferably n=2.32)

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

silver (Ag)

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

silicon zirconium nitride ( $\text{SiZrN}_x$ ) ( $n=2.2-2.45$ , preferably  $n=2.32$ )

silicon nitride (e.g.,  $\text{Si}_3\text{N}_4$ ) ( $n=1.8$  to  $2.0$ , preferably  $n=2.0$ )

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

silver (Ag)

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

silicon nitride (e.g.,  $\text{Si}_3\text{N}_4$ ) ( $n=1.8$  to  $2.0$ , preferably  $n=2.0$ )

air ( $n=1.0$ )

**[0069]** By using the silicon zirconium nitride and silicon nitride dielectric layers as shown in this embodiment, the layer system can be characterized by the top dielectric portion T having an effective index of refraction  $n$  less than that of middle dielectric portion M, which in turn has an effective index of refraction  $n$  less than that of the bottom dielectric portion B. In other words,  $n_T < n_M < n_B$ , where  $n_T$  is the effective index of refraction of the top dielectric portion T,  $n_M$  is the effective index of refraction of the middle dielectric portion M, and  $n_B$  is the effective index of refraction of the bottom dielectric portion B. Each of the top, middle and bottom dielectric portions T, M and B, respectively, can include a plurality of different dielectric layers, although in alternative embodiments any or all of these portions need only include a single dielectric layer. By gradually decreasing the respective effective indices of refraction " $n$ " from the innermost or bottom dielectric portion B, to the middle dielectric portion M, and on to the top dielectric portion T toward the air, the anti-reflection system of this embodiment enables increased visible transmission to be achieved. Surprisingly, the anti-reflection system may also enable fairly neutral color of the coated article in certain example embodiments.

## EXAMPLE(S) OF FIG. 11 EMBODIMENT

[0070] The Tables below illustrate Example 1 of the Fig. 11 embodiment, compared to a Comparative Example(s) (CE) similar to Fig. 1 of the instant application. The CE relates to a coating that is similar to that illustrated in the 09/794,224 application. The thicknesses for each of the layers in the First Table below are in angstroms (Å). The Second Table below sets forth the optical characteristics (e.g., visible transmission, color, etc.) for Example 1 and the CE based upon being annealed and in monolithic form.

FIRST TABLE: LAYER STRUCTURE – thicknesses (Fig. 11 embodiment)

	CE	Ex. 1
Glass		
SiZrN <sub>x</sub>	0Å	360Å
TiO <sub>2</sub>	125Å	0Å
Si <sub>3</sub> N <sub>4</sub>	165Å	0Å
NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	16Å
SiZrN <sub>x</sub>	0Å	229Å
SnO <sub>2</sub>	672Å	0Å
Si <sub>3</sub> N <sub>4</sub>	165Å	684Å
NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	16Å
SiZrN <sub>x</sub>	0Å	0Å
SnO <sub>2</sub>	227Å	0Å

Si <sub>3</sub> N <sub>4</sub>	252Å	404Å
SiO <sub>x</sub> N <sub>y</sub>	0Å	0Å
SiO <sub>2</sub>	0Å	0Å
Total diel:	1606Å	1677 Å

SECOND TABLE: OPTICAL PERFORMANCE (Fig. 11 embodiment; monolithic)

	T <sub>vis</sub>	a* <sub>t</sub>	b* <sub>t</sub>	R <sub>glass side (g)</sub>	a* <sub>g</sub>	b* <sub>g</sub>	R <sub>film side (f)</sub>	a* <sub>f</sub>	b* <sub>f</sub>
Ex. 1:	77.3%	-2.6	3.4	4.5%	9.0	-12.3	4.1%	3.9	-2.7
CE:	75.5%	-2.1	0.2	5.9%	9.2	-10.6	5.2%	3.2	-1.0

[0071] It can be seen from the Tables above regarding the Fig. 11 embodiment of this invention, that the anti-reflection system of the instant invention enables not only better visible transmission characteristics (i.e., increased visible transmission T<sub>vis</sub> %), but also reduced reflection (e.g., lower glass side reflection and/or film side visible reflection). In particular, Example 1 (see Fig. 11) had better visible transmission (higher T<sub>vis</sub>) and better glass and/or film side reflection (lower R<sub>g</sub> and/or R<sub>f</sub>) than the Comparative Example (CE – see Fig. 1). Surprisingly, Example 1 also had fairly neutral color.

[0072] Figure 12 is a cross sectional view of a coated article according to another embodiment of this invention. The Fig. 12 embodiment differs from Fig. 1 in that (a) the bottom titanium oxide and silicon nitride layers in bottom portion B of Fig. 1 have been removed and replaced with a layer of or including niobium oxide (stoichiometric Nb<sub>2</sub>O<sub>5</sub>, or some non-stoichiometric form), (b) the silicon nitride layer in the middle portion M of Fig. 1 has been removed, (c) a layer of or including niobium oxide (stoichiometric Nb<sub>2</sub>O<sub>5</sub>, or some non-stoichiometric form) has been added to the middle dielectric portion M in Fig. 12, and (d) the top silicon nitride layer in top portion T in Fig. 1 has been replaced with a layer of or including silicon oxide (stoichiometric or non-stoichiometric) in Fig. 12. The coated article of Fig. 12 includes from the glass substrate outwardly (all indices n at 550 nm):

glass ( $n=1.51$ )

niobium oxide (e.g.,  $\text{Nb}_2\text{O}_5$ ) ( $n=2.25-2.5$ , preferably  $n=2.33$ )

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

silver (Ag)

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

niobium oxide (e.g.,  $\text{Nb}_2\text{O}_5$ ) ( $n=2.25-2.5$ , preferably  $n=2.33$ )

tin oxide (e.g.,  $\text{SnO}_2$ ) ( $n=1.8$  to  $2.2$ , preferably  $n=2.0$ )

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

silver (Ag)

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

niobium oxide (e.g.,  $\text{Nb}_2\text{O}_5$ ) ( $n=2.25-2.5$ , preferably  $n=2.33$ )

tin oxide (e.g.,  $\text{SnO}_2$ ) ( $n=1.8$  to  $2.2$ , preferably  $n=2.0$ )

silicon oxide (e.g.,  $\text{SiO}_2$ ) ( $n=1.4$  to  $1.7$ , preferably  $n=1.45$ )

air ( $n=1.0$ )

**[0073]** By using the niobium oxide, silicon oxide, and tin oxide dielectric layers as shown in this embodiment, the layer system can be characterized by the top dielectric portion T having an effective index of refraction  $n$  less than that of middle dielectric portion M, which in turn has an effective index of refraction  $n$  less than that of the bottom dielectric portion B. In other words,  $n_T < n_M < n_B$ , where  $n_T$  is the effective index of refraction of the top dielectric portion T,  $n_M$  is the effective index of refraction of the middle dielectric portion M, and  $n_B$  is the effective index of refraction of the bottom dielectric portion B. Each of the top, middle and bottom dielectric portions T, M and B, respectively, can include a plurality of different dielectric layers, although in alternative embodiments any or all of these portions need only include a single dielectric layer. By gradually decreasing the respective effective indices of refraction "n" from the innermost or bottom dielectric portion B, to the middle dielectric portion M, and on to the top dielectric portion T toward the air, the anti-reflection system of this embodiment enables increased visible transmission to be

achieved. Surprisingly, the anti-reflection system may also enable fairly neutral color of the coated article in certain example embodiments.

#### EXAMPLE(S) OF FIG. 12 EMBODIMENT

[0074] The Tables below illustrate Example 1 of the Fig. 12 embodiment, compared to a Comparative Example(s) (CE) similar to Fig. 1 of the instant application. The CE relates to a coating that is similar to that illustrated in the 09/794,224 application. The thicknesses for each of the layers in the First Table below are in angstroms (Å). The Second Table below sets forth the optical characteristics (e.g., visible transmission, color, etc.) for Example 1 and the CE based upon being annealed and in monolithic form.

FIRST TABLE: LAYER STRUCTURE – thicknesses (Fig. 12 embodiment)

	CE	Ex. 1
Glass		
Nb <sub>x</sub> O <sub>y</sub>	0Å	342Å
TiO <sub>2</sub>	125Å	0Å
Si <sub>3</sub> N <sub>4</sub>	165Å	0Å
NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	16Å
Nb <sub>x</sub> O <sub>y</sub>	0Å	640Å
SnO <sub>2</sub>	672Å	96Å
Si <sub>3</sub> N <sub>4</sub>	165Å	0Å
NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	16Å



Nb <sub>x</sub> O <sub>y</sub>	0Å	222Å
SnO <sub>2</sub>	227Å	37Å
Si <sub>3</sub> N <sub>4</sub>	252Å	0Å
SiO <sub>x</sub> N <sub>y</sub>	0Å	0Å
SiO <sub>2</sub>	0Å	372Å
Total diel:	1606Å	1709 Å

SECOND TABLE: OPTICAL PERFORMANCE (Fig. 12 embodiment; monolithic)

	T <sub>vis</sub>	a* <sub>t</sub>	b* <sub>t</sub>	R <sub>glass side (g)</sub>	a* <sub>g</sub>	b* <sub>g</sub>	R <sub>film side (f)</sub>	a* <sub>f</sub>	b* <sub>f</sub>
Ex. 1:	78.5%	-1.3	-0.3	4.6%	8.2	-8.6	4.0%	3.7	-2.4
CE:	75.5%	-2.1	0.2	5.9%	9.2	-10.6	5.2%	3.2	-1.0

**[0075]** It can be seen from the Tables above regarding the Fig. 12 embodiment of this invention, that the anti-reflection system of the instant invention enables not only better visible transmission characteristics (i.e., increased visible transmission T<sub>vis</sub> %), but also reduced reflection (e.g., lower glass side reflection and/or film side visible reflection). In particular, Example 1 (see Fig. 12) had better visible transmission (higher T<sub>vis</sub>) and better glass and/or film side reflection (lower R<sub>g</sub> and/or R<sub>f</sub>) than the Comparative Example (CE – see Fig. 1). Surprisingly, Example 1 also had more neutral transmissive and glass side reflective color than the CE.

**[0076]** Figure 13 is a cross sectional view of a coated article according to another embodiment of this invention. The Fig. 13 embodiment differs from the Fig. 12 embodiment in that the top silicon oxide and niobium oxide layers in top dielectric portion T of Fig. 12 have been removed. The coated article of Fig. 13 includes from the glass substrate outwardly (all indices n at 550 nm):

glass (n=1.51)

niobium oxide (e.g., Nb<sub>2</sub>O<sub>5</sub>) (n=2.25-2.5, preferably n=2.33)

nickel-chromium-oxide (NiCrO<sub>x</sub>)

silver (Ag)

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

niobium oxide (e.g.,  $\text{Nb}_2\text{O}_5$ ) ( $n=2.25$ - $2.5$ , preferably  $n=2.33$ )

tin oxide (e.g.,  $\text{SnO}_2$ ) ( $n=1.8$  to  $2.2$ , preferably  $n=2.0$ )

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

silver (Ag)

nickel-chromium-oxide ( $\text{NiCrO}_x$ )

tin oxide (e.g.,  $\text{SnO}_2$ ) ( $n=1.8$  to  $2.2$ , preferably  $n=2.0$ )

air ( $n=1.0$ )

**[0077]** By using the niobium oxide and tin oxide dielectric layers as shown in this embodiment, the layer system can be characterized by the top dielectric portion T having an effective index of refraction  $n$  less than that of middle dielectric portion M, which in turn has an effective index of refraction  $n$  less than that of the bottom dielectric portion B. In other words,  $n_T < n_M < n_B$ , where  $n_T$  is the effective index of refraction of the top dielectric portion T,  $n_M$  is the effective index of refraction of the middle dielectric portion M, and  $n_B$  is the effective index of refraction of the bottom dielectric portion B. Each of the top, middle and bottom dielectric portions T, M and B, respectively, can include a plurality of different dielectric layers, although in alternative embodiments any or all of these portions need only include a single dielectric layer. By gradually decreasing the respective effective indices of refraction " $n$ " from the innermost or bottom dielectric portion B, to the middle dielectric portion M, and on to the top dielectric portion T toward the air, the anti-reflection system of this embodiment enables increased visible transmission to be achieved. Surprisingly, the anti-reflection system may also enable fairly neutral color of the coated article in certain example embodiments.

#### EXAMPLE(S) OF FIG. 13 EMBODIMENT

**[0078]** The Tables below illustrate Example 1 of the Fig. 13 embodiment, compared to a Comparative Example(s) (CE) similar to Fig. 1 of the instant application. The CE relates to a coating that is similar to that illustrated in the

09/794,224 application. The thicknesses for each of the layers in the First Table below are in angstroms (Å). The Second Table below sets forth the optical characteristics (e.g., visible transmission, color, etc.) for Example 1 and the CE based upon being annealed and in monolithic form.

FIRST TABLE: LAYER STRUCTURE – thicknesses (Fig. 13 embodiment)

	CE	Ex. 1
Glass		
Nb <sub>x</sub> O <sub>y</sub>	0Å	347Å
TiO <sub>2</sub>	125Å	0Å
Si <sub>3</sub> N <sub>4</sub>	165Å	0Å
NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	16Å
Nb <sub>x</sub> O <sub>y</sub>	0Å	639Å
SnO <sub>2</sub>	672Å	90Å
Si <sub>3</sub> N <sub>4</sub>	165Å	0Å
NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	16Å
Nb <sub>x</sub> O <sub>y</sub>	0Å	0Å
SnO <sub>2</sub>	227Å	428Å
Si <sub>3</sub> N <sub>4</sub>	252Å	0Å
SiO <sub>x</sub> N <sub>y</sub>	0Å	0Å
SiO <sub>2</sub>	0Å	0Å
Total diel:	1606Å	1504 Å

SECOND TABLE: OPTICAL PERFORMANCE (Fig. 13 embodiment; monolithic)

	$T_{vis}$	$a^*_t$	$b^*_t$	$R_{glass\ side\ (g)}$	$a^*_g$	$b^*_g$	$R_{film\ side\ (f)}$	$a^*_f$	$b^*_f$
Ex. 1:	78.4%	-1.5	0.1	4.6%	9.0	-9.9	4.1%	3.2	-2.6
CE:	75.5%	-2.1	0.2	5.9%	9.2	-10.6	5.2%	3.2	-1.0

**[0079]** It can be seen from the Tables above regarding the Fig. 13 embodiment of this invention, that the anti-reflection system of the instant invention enables not only better visible transmission characteristics (i.e., increased visible transmission  $T_{vis}$  %), but also reduced reflection (e.g., lower glass side reflection and/or film side visible reflection). In particular, Example 1 (see Fig. 13) had better visible transmission (higher  $T_{vis}$ ) and better glass and/or film side reflection (lower  $R_g$  and/or  $R_f$ ) than the Comparative Example (CE – see Fig. 1). Surprisingly, Example 1 also had more neutral transmissive and glass side reflective color than the CE.

**[0080]** Figure 14 is a cross sectional view of a coated article according to another embodiment of this invention. The Fig. 14 embodiment differs from the Fig. 13 embodiment in that the top tin oxide layer of Fig. 13 has been replaced with a silicon nitride inclusive layer in Fig. 14. The coated article of Fig. 14 includes from the glass substrate outwardly (all indices  $n$  at 550 nm):

glass ( $n=1.51$ )

niobium oxide (e.g.,  $Nb_2O_5$ ) ( $n=2.25-2.5$ , preferably  $n=2.33$ )

nickel-chromium-oxide ( $NiCrO_x$ )

silver (Ag)

nickel-chromium-oxide ( $NiCrO_x$ )

niobium oxide (e.g.,  $Nb_2O_5$ ) ( $n=2.25-2.5$ , preferably  $n=2.33$ )

tin oxide (e.g.,  $SnO_2$ ) ( $n=1.8$  to  $2.2$ , preferably  $n=2.0$ )

nickel-chromium-oxide ( $NiCrO_x$ )

silver (Ag)

nickel-chromium-oxide ( $NiCrO_x$ )

silicon nitride (e.g.,  $\text{Si}_3\text{N}_4$ ) ( $n=1.8$  to  $2.0$ , preferably  $n=2.0$ )

air ( $n=1.0$ )

[0081] By using the niobium oxide, silicon nitride, and tin oxide dielectric layers as shown in this embodiment, the layer system can be characterized by the top dielectric portion T having an effective index of refraction  $n$  less than that of middle dielectric portion M, which in turn has an effective index of refraction  $n$  less than that of the bottom dielectric portion B. In other words,  $n_T < n_M < n_B$ , where  $n_T$  is the effective index of refraction of the top dielectric portion T,  $n_M$  is the effective index of refraction of the middle dielectric portion M, and  $n_B$  is the effective index of refraction of the bottom dielectric portion B. Each of the top, middle and bottom dielectric portions T, M and B, respectively, can include a plurality of different dielectric layers, although in alternative embodiments any or all of these portions need only include a single dielectric layer. By gradually decreasing the respective effective indices of refraction " $n$ " from the innermost or bottom dielectric portion B, to the middle dielectric portion M, and on to the top dielectric portion T toward the air, the anti-reflection system of this embodiment enables increased visible transmission to be achieved. Surprisingly, the anti-reflection system may also enable fairly neutral color of the coated article in certain example embodiments.

#### EXAMPLE(S) OF FIG. 14 EMBODIMENT

[0082] The Tables below illustrate Example 1 of the Fig. 14 embodiment, compared to a Comparative Example(s) (CE) similar to Fig. 1 of the instant application. The CE relates to a coating that is similar to that illustrated in the 09/794,224 application. The thicknesses for each of the layers in the First Table below are in angstroms ( $\text{\AA}$ ). The Second Table below sets forth the optical characteristics (e.g., visible transmission, color, etc.) for Example 1 and the CE based upon being annealed and in monolithic form.

FIRST TABLE: LAYER STRUCTURE – thicknesses (Fig. 14 embodiment)

	CE	Ex. 1
Glass		
Nb <sub>x</sub> O <sub>y</sub>	0Å	344Å
TiO <sub>2</sub>	125Å	0Å
Si <sub>3</sub> N <sub>4</sub>	165Å	0Å
NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	16Å
Nb <sub>x</sub> O <sub>y</sub>	0Å	641Å
SnO <sub>2</sub>	672Å	89Å
Si <sub>3</sub> N <sub>4</sub>	165Å	0Å
NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	16Å
Nb <sub>x</sub> O <sub>y</sub>	0Å	0Å
SnO <sub>2</sub>	227Å	0Å
Si <sub>3</sub> N <sub>4</sub>	252Å	428Å
SiO <sub>x</sub> N <sub>y</sub>	0Å	0Å
SiO <sub>2</sub>	0Å	0Å
Total diel:	1606Å	1502 Å

SECOND TABLE: OPTICAL PERFORMANCE (Fig. 14 embodiment; monolithic)

	T <sub>vis</sub>	a* <sub>t</sub>	b* <sub>t</sub>	R <sub>glass side (g)</sub>	a* <sub>g</sub>	b* <sub>g</sub>	R <sub>film side (f)</sub>	a* <sub>f</sub>	b* <sub>f</sub>
Ex. 1:	78.3%	-1.4	0.0	4.6%	8.7	-9.3	4.1%	3.4	-2.5

CE: 75.5% -2.1 0.2 5.9% 9.2 -10.6 5.2% 3.2 -1.0

**[0083]** It can be seen from the Tables above regarding the Fig. 14 embodiment of this invention, that the anti-reflection system of the instant invention enables not only better visible transmission characteristics (i.e., increased visible transmission  $T_{vis}$  %), but also reduced reflection (e.g., lower glass side reflection and/or film side visible reflection). In particular, Example 1 (see Fig. 14) had better visible transmission (higher  $T_{vis}$ ) and better glass and/or film side reflection (lower  $R_g$  and/or  $R_f$ ) than the Comparative Example (CE – see Fig. 1). Surprisingly, Example 1 also had more neutral transmissive and glass side reflective color than the CE.

**[0084]** Figure 15 is a cross sectional view of a coated article according to another embodiment of this invention. The Fig. 15 embodiment differs from the Fig. 12 embodiment in that the two upper nickel chrome oxide contact layers have been removed from the Fig. 12 embodiment. The coated article of Fig. 15 includes from the glass substrate outwardly (all indices  $n$  at 550 nm):

glass ( $n=1.51$ )

niobium oxide (e.g.,  $Nb_2O_5$ ) ( $n=2.25-2.5$ , preferably  $n=2.33$ )

nickel-chromium-oxide ( $NiCrO_x$ )

silver (Ag)

niobium oxide (e.g.,  $Nb_2O_5$ ) ( $n=2.25-2.5$ , preferably  $n=2.33$ )

tin oxide (e.g.,  $SnO_2$ ) ( $n=1.8$  to  $2.2$ , preferably  $n=2.0$ )

nickel-chromium-oxide ( $NiCrO_x$ )

silver (Ag)

niobium oxide (e.g.,  $Nb_2O_5$ ) ( $n=2.25-2.5$ , preferably  $n=2.33$ )

tin oxide (e.g.,  $SnO_2$ ) ( $n=1.8$  to  $2.2$ , preferably  $n=2.0$ )

silicon oxide (e.g.,  $SiO_2$ ) ( $n=1.4$  to  $1.7$ , preferably  $n=1.45$ )

air ( $n=1.0$ )

**[0085]** By using the niobium oxide, silicon oxide, and tin oxide dielectric layers as shown in this embodiment, the layer system can be characterized by the top

dielectric portion T having an effective index of refraction  $n$  less than that of middle dielectric portion M, which in turn has an effective index of refraction  $n$  less than that of the bottom dielectric portion B. In other words,  $n_T < n_M < n_B$ , where  $n_T$  is the effective index of refraction of the top dielectric portion T,  $n_M$  is the effective index of refraction of the middle dielectric portion M, and  $n_B$  is the effective index of refraction of the bottom dielectric portion B. Each of the top, middle and bottom dielectric portions T, M and B, respectively, can include a plurality of different dielectric layers, although in alternative embodiments any or all of these portions need only include a single dielectric layer. By gradually decreasing the respective effective indices of refraction " $n$ " from the innermost or bottom dielectric portion B, to the middle dielectric portion M, and on to the top dielectric portion T toward the air, the anti-reflection system of this embodiment enables increased visible transmission to be achieved. Surprisingly, the anti-reflection system may also enable fairly neutral color of the coated article in certain example embodiments.

#### EXAMPLE(S) OF FIG. 15 EMBODIMENT

**[0086]** The Tables below illustrate Example 1 of the Fig. 15 embodiment, compared to a Comparative Example(s) (CE) similar to Fig. 1 of the instant application. The CE relates to a coating that is similar to that illustrated in the 09/794,224 application. The thicknesses for each of the layers in the First Table below are in angstroms (Å). The Second Table below sets forth the optical characteristics (e.g., visible transmission, color, etc.) for Example 1 and the CE based upon being annealed and in monolithic form.

FIRST TABLE: LAYER STRUCTURE – thicknesses (Fig. 15 embodiment)

	CE	Ex. 1
Glass		
Nb <sub>x</sub> O <sub>y</sub>	0Å	337Å
TiO <sub>2</sub>	125Å	0Å
Si <sub>3</sub> N <sub>4</sub>	165Å	0Å



NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	0Å
Nb <sub>x</sub> O <sub>y</sub>	0Å	564Å
SnO <sub>2</sub>	672Å	169Å
Si <sub>3</sub> N <sub>4</sub>	165Å	0Å
NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	0Å
Nb <sub>x</sub> O <sub>y</sub>	0Å	209Å
SnO <sub>2</sub>	227Å	50Å
Si <sub>3</sub> N <sub>4</sub>	252Å	0Å
SiO <sub>x</sub> N <sub>y</sub>	0Å	0Å
SiO <sub>2</sub>	0Å	379Å
Total diel:	1606Å	1708 Å

SECOND TABLE: OPTICAL PERFORMANCE (Fig. 15 embodiment; monolithic)

	T <sub>vis</sub>	a* <sub>t</sub>	b* <sub>t</sub>	R <sub>glass side (g)</sub>	a* <sub>g</sub>	b* <sub>g</sub>	R <sub>film side (f)</sub>	a* <sub>f</sub>	b* <sub>f</sub>
Ex. 1:	82.1%	-1.1	-0.8	4.5%	4.0	-3.9	3.8%	1.4	-1.8
CE:	75.5%	-2.1	0.2	5.9%	9.2	-10.6	5.2%	3.2	-1.0

[0087] It can be seen from the Tables above regarding the Fig. 15 embodiment of this invention, that the anti-reflection system of the instant invention enables not only better visible transmission characteristics (i.e., increased visible transmission T<sub>vis</sub> %), but also reduced reflection (e.g., lower glass side reflection and/or film side visible reflection). In particular, Example 1 (see Fig. 15) had better visible transmission (higher T<sub>vis</sub>) and better glass and/or film side reflection (lower R<sub>g</sub> and/or

$R_f$ ) than the Comparative Example (CE – see Fig. 1). Surprisingly, Example 1 also had more neutral color than the CE.

**[0088]** Figure 16 is a cross sectional view of a coated article according to another embodiment of this invention. The Fig. 16 embodiment differs from the Fig. 15 embodiment in that the upper silicon oxide and tin oxide layers in top dielectric portion T have been replaced with a layer of or including silicon oxynitride. The coated article of Fig. 16 includes from the glass substrate outwardly (all indices  $n$  at 550 nm):

glass ( $n=1.51$ )

niobium oxide (e.g.,  $Nb_2O_5$ ) ( $n=2.25$ -2.5, preferably  $n=2.33$ )

nickel-chromium-oxide ( $NiCrO_x$ )

silver (Ag)

niobium oxide (e.g.,  $Nb_2O_5$ ) ( $n=2.25$ -2.5, preferably  $n=2.33$ )

tin oxide (e.g.,  $SnO_2$ ) ( $n=1.8$  to 2.2, preferably  $n=2.0$ )

nickel-chromium-oxide ( $NiCrO_x$ )

silver (Ag)

niobium oxide (e.g.,  $Nb_2O_5$ ) ( $n=2.25$ -2.5, preferably  $n=2.33$ )

silicon oxynitride (e.g.,  $SiO_xN_y$ ) ( $n=1.45$ -2.0, preferably  $n=1.6$ -1.9)

air ( $n=1.0$ )

**[0089]** By using the niobium oxide, silicon oxynitride, and tin oxide dielectric layers as shown in this embodiment, the layer system can be characterized by the top dielectric portion T having an effective index of refraction  $n$  less than that of middle dielectric portion M, which in turn has an effective index of refraction  $n$  less than that of the bottom dielectric portion B. In other words,  $n_T < n_M < n_B$ , where  $n_T$  is the effective index of refraction of the top dielectric portion T,  $n_M$  is the effective index of refraction of the middle dielectric portion M, and  $n_B$  is the effective index of refraction of the bottom dielectric portion B. Each of the top, middle and bottom dielectric portions T, M and B, respectively, can include a plurality of different

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dielectric layers, although in alternative embodiments any or all of these portions need only include a single dielectric layer. By gradually decreasing the respective effective indices of refraction "n" from the innermost or bottom dielectric portion B, to the middle dielectric portion M, and on to the top dielectric portion T toward the air, the anti-reflection system of this embodiment enables increased visible transmission to be achieved. Surprisingly, the anti-reflection system may also enable fairly neutral color of the coated article in certain example embodiments. The silicon oxynitride layer is beneficial in that its index of refraction n (at 550 nm) can be varied from 1.45 to 2.0, more preferably from 1.6 to 1.9, and most preferably from 1.65 to 1.85, in different embodiments of this invention. In this and all other silicon oxynitride inclusive embodiments herein, the silicon oxynitride layer may have a constant (or approximately constant, i.e., constant plus/minus about 5%) index of refraction n throughout its entire thickness in certain embodiments of this invention, but alternatively may be oxidation and/or nitride graded so as to have an index of refraction n which varies through the thickness of the layer (e.g., the index n may gradually decrease through the thickness of the silicon oxynitride layer moving toward the air).

EXAMPLE(S) OF FIG. 16 EMBODIMENT

[0090] The Tables below illustrate Example 1 of the Fig. 16 embodiment, compared to a Comparative Example(s) (CE) similar to Fig. 1 of the instant application. The CE relates to a coating that is similar to that illustrated in the 09/794,224 application. The thicknesses for each of the layers in the First Table below are in angstroms (Å). The Second Table below sets forth the optical characteristics (e.g., visible transmission, color, etc.) for Example 1 and the CE based upon being annealed and in monolithic form.

FIRST TABLE: LAYER STRUCTURE – thicknesses (Fig. 16 embodiment)

	CE	Ex. 1
Glass		
Nb <sub>x</sub> O <sub>y</sub>	0Å	342Å

TiO <sub>2</sub>	125Å	0Å
Si <sub>3</sub> N <sub>4</sub>	165Å	0Å
NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	0Å
Nb <sub>x</sub> O <sub>y</sub>	0Å	554Å
SnO <sub>2</sub>	672Å	188Å
Si <sub>3</sub> N <sub>4</sub>	165Å	0Å
NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	0Å
Nb <sub>x</sub> O <sub>y</sub>	0Å	182Å
SnO <sub>2</sub>	227Å	0Å
Si <sub>3</sub> N <sub>4</sub>	252Å	0Å
SiO <sub>x</sub> N <sub>y</sub>	0Å	336Å
SiO <sub>2</sub>	0Å	0Å
Total diel:	1606Å	1602 Å

SECOND TABLE: OPTICAL PERFORMANCE (Fig. 16 embodiment; monolithic)

	T <sub>vis</sub>	a* <sub>t</sub>	b* <sub>t</sub>	R <sub>glass side (g)</sub>	a* <sub>g</sub>	b* <sub>g</sub>	R <sub>film side (f)</sub>	a* <sub>f</sub>	b* <sub>f</sub>
Ex. 1:	82.0%	-1.1	-0.7	4.6%	4.5	-4.6	3.9%	1.5	-1.8
CE:	75.5%	-2.1	0.2	5.9%	9.2	-10.6	5.2%	3.2	-1.0

[0091] It can be seen from the Tables above regarding the Fig. 16 embodiment of this invention, that the anti-reflection system of the instant invention enables not only better visible transmission characteristics (i.e., increased visible transmission T<sub>vis</sub> %), but also reduced reflection (e.g., lower glass side reflection and/or film side

visible reflection). In particular, Example 1 (see Fig. 16) had better visible transmission (higher  $T_{vis}$ ) and better glass and/or film side reflection (lower  $R_g$  and/or  $R_f$ ) than the Comparative Example (CE – see Fig. 1). Surprisingly, Example 1 also had more neutral color than the CE (especially glass side reflective color).

**[0092]** Figure 17 is a cross sectional view of a coated article according to another embodiment of this invention. The Fig. 17 embodiment differs from the Fig. 14 embodiment in that an additional niobium oxide layer has been added to the top dielectric portion T, and the two top contact layers were NiCr (i.e. not significantly oxidized). The coated article of Fig. 17 includes from the glass substrate outwardly (all indices n at 550 nm):

glass ( $n=1.51$ )

niobium oxide (e.g.,  $Nb_2O_5$ ) ( $n=2.25-2.5$ , preferably  $n=2.33$ )

nickel-chromium-oxide ( $NiCrO_x$ )

silver (Ag)

nickel-chromium (NiCr)

niobium oxide (e.g.,  $Nb_2O_5$ ) ( $n=2.25-2.5$ , preferably  $n=2.33$ )

tin oxide (e.g.,  $SnO_2$ ) ( $n=1.8$  to  $2.2$ , preferably  $n=2.0$ )

nickel-chromium-oxide ( $NiCrO_x$ )

silver (Ag)

nickel-chromium (NiCr)

niobium oxide (e.g.,  $Nb_2O_5$ ) ( $n=2.25-2.5$ , preferably  $n=2.33$ )

silicon nitride (e.g.,  $Si_3N_4$ ) ( $n=1.8$  to  $2.0$ , preferably  $n=2.0$ )

air ( $n=1.0$ )

**[0093]** By using the niobium oxide, silicon nitride, and tin oxide dielectric layers as shown in this embodiment, the layer system can be characterized by the top dielectric portion T having an effective index of refraction n less than or equal to that of middle dielectric portion M, which in turn has an effective index of refraction n less than or equal to that of the bottom dielectric portion B. In other words,

$n_T \leq n_M \leq n_B$ , where  $n_T$  is the effective index of refraction of the top dielectric portion T,  $n_M$  is the effective index of refraction of the middle dielectric portion M, and  $n_B$  is the effective index of refraction of the bottom dielectric portion B. Each of the top, middle and bottom dielectric portions T, M and B, respectively, can include a plurality of different dielectric layers, although in alternative embodiments any or all of these portions need only include a single dielectric layer. By gradually decreasing the respective effective indices of refraction "n" from the innermost or bottom dielectric portion B, to the middle dielectric portion M, and on to the top dielectric portion T toward the air, the anti-reflection system of this embodiment enables increased visible transmission to be achieved. Surprisingly, the anti-reflection system may also enable fairly neutral color of the coated article in certain example embodiments. While the two upper contact layers were NiCr (not significantly oxidized) in this embodiment, it will be recognized by those skilled in the art that in other embodiments of this invention these NiCr contact layers may be nitrided.

#### EXAMPLE(S) OF FIG. 17 EMBODIMENT

[0094] The Tables below illustrate Example 1 of the Fig. 17 embodiment, compared to a Comparative Example(s) (CE) similar to Fig. 1 of the instant application. The CE relates to a coating that is similar to that illustrated in the 09/794,224 application. The thicknesses for each of the layers in the First Table below are in angstroms (Å). The Second Table below sets forth the optical characteristics (e.g., visible transmission, color, etc.) for Example 1 and the CE based upon being annealed and in monolithic form.

FIRST TABLE: LAYER STRUCTURE – thicknesses (Fig. 17 embodiment)

	CE	Ex. 1
Glass		
Nb <sub>x</sub> O <sub>y</sub>	0Å	346Å
TiO <sub>2</sub>	125Å	0Å
Si <sub>3</sub> N <sub>4</sub>	165Å	0Å

NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	0Å
NiCr	0Å	3Å
Nb <sub>x</sub> O <sub>y</sub>	0Å	652Å
SnO <sub>2</sub>	672Å	108Å
Si <sub>3</sub> N <sub>4</sub>	165Å	0Å
NiCrO <sub>x</sub>	18Å	18Å
Ag	98Å	98Å
NiCrO <sub>x</sub>	16Å	0Å
NiCr	0Å	3Å
Nb <sub>x</sub> O <sub>y</sub>	0Å	88Å
SnO <sub>2</sub>	227Å	0Å
Si <sub>3</sub> N <sub>4</sub>	252Å	350Å
SiO <sub>x</sub> N <sub>y</sub>	0Å	0Å
SiO <sub>2</sub>	0Å	0Å
Total diel:	1606Å	1544 Å

SECOND TABLE: OPTICAL PERFORMANCE (Fig. 17 embodiment; monolithic)

	$T_{vis}$	$a^*_t$	$b^*_t$	$R_{glass\ side\ (g)}$	$a^*_g$	$b^*_g$	$R_{film\ side\ (f)}$	$a^*_f$	$b^*_f$
Ex. 1:	77.3%	-1.8	-0.8	4.7%	10.3	-10.7	4.4%	4.1	-2.8
CE:	75.5%	-2.1	0.2	5.9%	9.2	-10.6	5.2%	3.2	-1.0

**[0095]** It can be seen from the Tables above regarding the Fig. 17 embodiment of this invention, that the anti-reflection system of the instant invention enables not

only better visible transmission characteristics (i.e., increased visible transmission  $T_{vis}$  %), but also reduced reflection (e.g., lower glass side reflection and/or film side visible reflection). In particular, Example 1 (see Fig. 17) had better visible transmission (higher  $T_{vis}$ ) and better glass and/or film side reflection (lower  $R_g$  and/or  $R_f$ ) than the Comparative Example (CE – see Fig. 1). Fairly neutral transmissive color was also provided in Example 1.

**[0096]** Accordingly, coated articles of certain example embodiments of this invention are characterized by one or more of the following parameters:

Characteristic	General	More Preferred	Most Preferred
$T_{vis}$ (Ill. C 2 deg.):	$\geq 70\%$	$\geq 75\%$	$\geq 76.5\%$
$R_gY$ (Ill. C, 2 deg.):	$\leq 11\%$	$\leq 9\%$	$\leq 5.0\%$
$R_fY$ (Ill. C; 2 deg.):	$\leq 11\%$	$\leq 9\%$	$\leq 5.0\%$
$T_{solar}$ :	$\leq 50\%$	$\leq 48\%$	

**[0097]** While the invention has been described in connection with what is presently considered to be the most practical and preferred embodiment, it is to be understood that the invention is not to be limited to the disclosed embodiment, but on the contrary, is intended to cover various modifications and equivalent arrangements included within the spirit and scope of the appended claims. For example and without limitation, materials other than those described above may be used in other embodiments of this invention without departing from the spirit of this invention. For example and without limitation, silicon oxide layers may be at least partially nitrided in certain embodiments, and silicon nitride layers may be at least partially oxidized in certain embodiments.